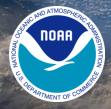
Tropical Cyclone Intensity Analysis and Forecasting

Mark DeMaria National Hurricane Center

WMO RA-IV Workshop on Hurricane Forecasting and Warning Miami, Florida 7 March 2017









- Estimating the Current Intensity (with Exercise)
- Factors that Influence Intensity Change
- Intensity Forecasting Models
- Official Intensity Forecasts
- Exercise



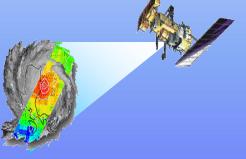


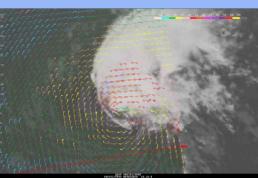
How Do We Estimate Intensity?

WEATHING SERVIC

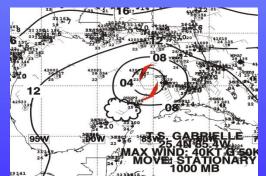
- Satellites (primary)
 - Geostationary infrared & visible images (Dvorak Technique)
 - Microwave soundings (AMSU)
 - Scatterometer derived surface winds (ASCAT)







- Surface observations
 - Ships, buoys, land stations (limited)





IDRR COMMAN

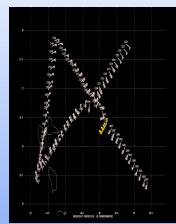


How Do We Estimate Intensity?

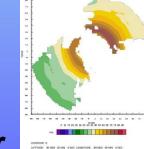
- Aircraft reconnaissance
 - Flight-level winds
 - GPS dropsondes



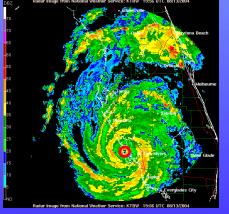


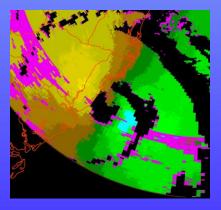


Stepped-Frequency Microwave Radiometer (SFMR)



- Doppler radar
 - Land-based (WSR-88D)
 - Airborne

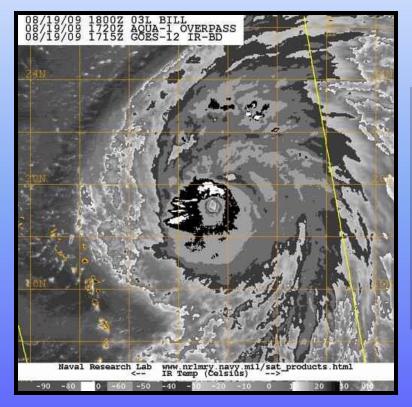






Exercise 1: Estimating the Current Intensity of Hurricane Bill





19 August 1800 UTC

Dvorak classification:

TAFB: **T6.5** = 127 kt SAB: **T6.0** = 115 kt

3-hr average ADT: **T6.4** = 125 kt





Dvorak Scale



CI	MWS	MSLP	MSLP
Number	(kt)	(Atlantic)	(NW Pacific)
1.0	25		
1.5	25		
2.0	30	1009 mb	1000 mb
2.5	35	1005 mb	997 mb
3.0	45	1000 mb	991 mb
3.5	55	994 mb	984 mb
4.0	65	987 mb	976 mb
4.5	77	979 mb	966 mb
5.0	90	970 mb	954 mb
5.5	102	960 mb	941 mb
6.0	115	948 mb	927 mb
6.5	127	935 mb	914 mb
7.0	140	921 mb	898 mb
7.5	155	906 mb	879 mb
8.0	170	890 mb	858 mb



Vortex Message



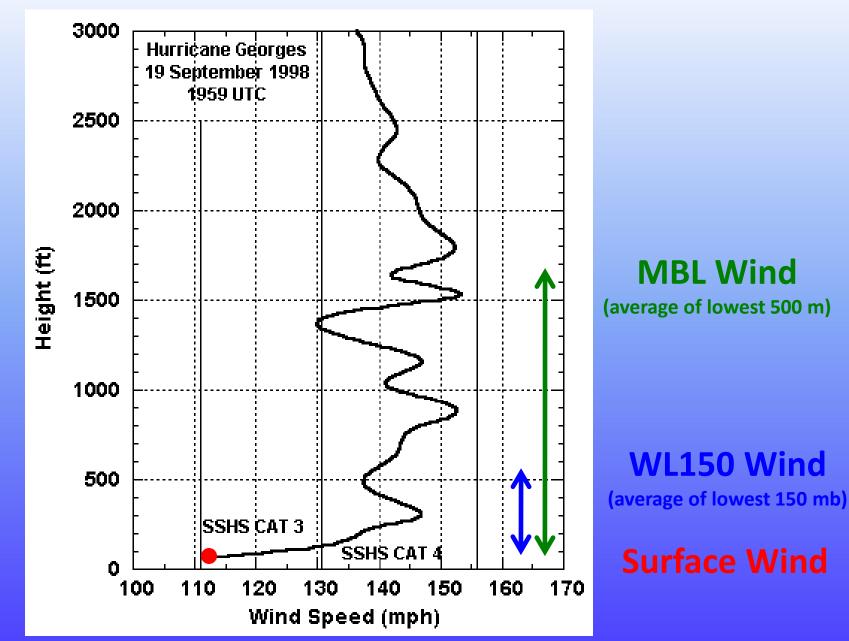


000 URNT12 KNHC 191819 CCA	A) Date/Time of center fix
VORTEX DATA MESSAGE AL032009	B) Center position
A. 19/17:57:30Z	C) Std surface/min height
B. 19 deg 16 min N O56 deg 55 min W	D) Max sfc wind (visually observed or SFMR)
C. 700 mb 2665 m	D) Max sic willa (visually observed of Srivik)
D. 102 kt SFMR surface wind	E) Bearing/range of (D) from center
E. 056 deg 24 nm	F) Max flt-lvl wind on inbound leg
F. 134 deg 135 kt G. 055 deg 27 nm	G) Bearing/range of (F)
H. 947 mb	H) Minimum pressure
I. 11 C / 3045 m	
J. 19 C / 3047 m 90% from 700 mb	I) Max flt-lvl temp outside eyewall/PA
K. 6 C / NA Surface estimate =	J) Max flt-lvl temp inside eye/PA
L. OPEN SW 0.9×135 kt = 122 kt	
n. coz	K) DPT/SST at (J)
N. 12345 / 07	L) Eyewall character (e.g., CLOSED)
0. 0.02 / 0.5 nm	
P. AF303 0203A BILL OB 12 CC	M) Eye diameter (nm)
MAX FL WIND 135 KT NE QUAD 17:48:30Z	N) Method of fix
;	
	O) Fix accuracy (NAV/MET)
	P) Remarks (includes outbound max)
	and a second sec



Dropsonde







Dropsonde

000 UZNT13 KNHC 192344 69237 99203 70578 07807 99955 25600 09122 00912 ///// ///// XXAA 92277 23801 10140 85016 20600 11641 70686 148// 14599 88999 77999 31313 09608 82322 61616 NOAA3 WX03A BILL4 OB 11 62626 REL 2033N05779W 232240 SPG 2042N05793W 232707 WL150 09134 0 86 DLM WND 12128 954696 MBL WND 10139 LST WND 011= 69238 99203 70578 07807 00955 25600 11941 24400 22920 23802 XXBB 33741 17000 44719 16001 55695 146// 21212 00955 09122 11952 08618 22943 09640 33938 09646 449 55916 10646 66896 11139 77749 13635 88740 14618 99695 150 200 31313 09608 82322 61616 NOAA3 WX03A BILL4 OB 11 62626 REL 2033N05779W 232240 SPG 2042N05793W 232707 WL150 175 86 DLM WND 12128 954696 MBL WND 10139 LST WND 011=

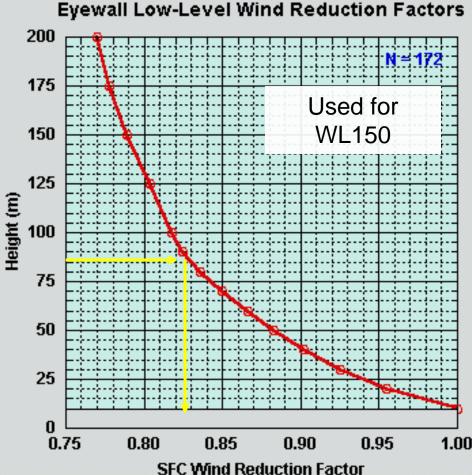
Northeast eyewall:

Surface = 122 kt (gust?)

MBL (lowest 500 m) = 139 × 0.8 = 111 k

WL150 (lowest 150 mb) = 134 × 0.83 = 111 kt







Determine the Official Intensity



We can only sample a part of the TC ach observation has strengths and weaknesses We want a value that is representative of the TC's circulation				
We can only cample a new of				
• OFCL at 1800 UTC:	115 kt			
 Drop sfc-adjusted MBL: 	111 kt			
 Drop sfc-adjusted WL150: 	111 kt			
 Dropsonde surface value: 	122 kt			
• Recon sfc-adjusted flight-level wind:	122 kt			
 SFMR surface wind 	102 kt			
Objective ADT:	125 kt			
 Subjective Dvorak: 	127 / 115 kt			

EXERCISE 1 Intensity Estimation



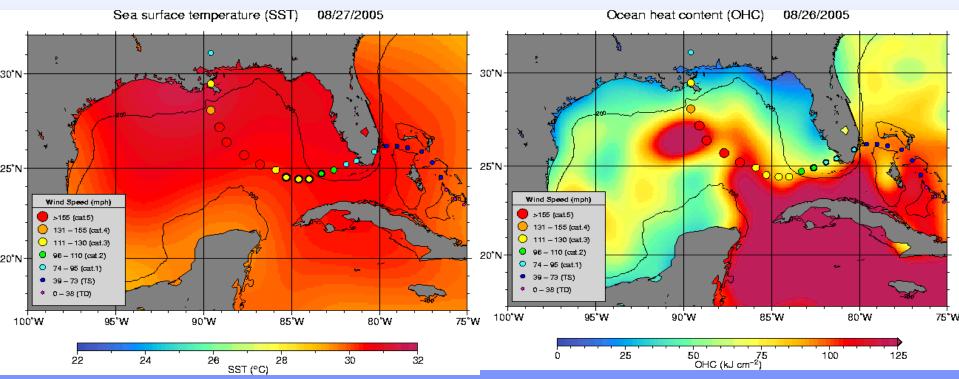


Factors Affecting Tropical Cyclone Intensity

- Sea surface temperature (SST) / upper ocean heat content (OHC)
- Environmental winds, esp. vertical wind shear
- Trough interactions
- Temperature and moisture patterns in the storm environment
- Internal effects (e.g. eyewall replacement cycles)
- Interaction with land

SST vs. OHC





Sea Surface Temperatures

only provides a view of the very top layer of the ocean.

Ocean Heat Content

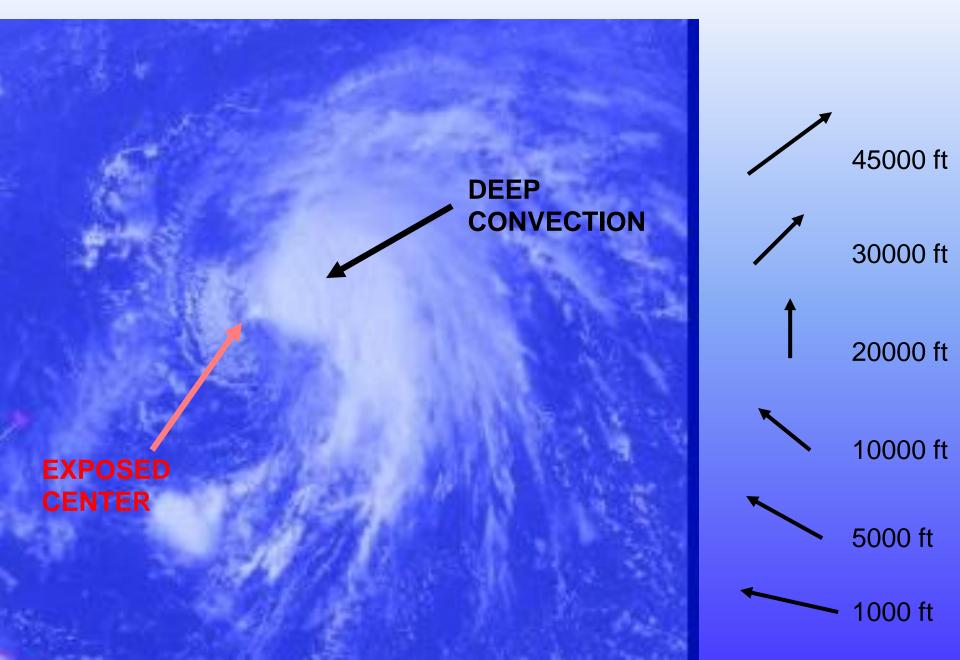
estimates the amount of heat available over a depth of warm water.

the greater the depth the more available heat that can be potentially converted to energy



Vertical Wind Shear

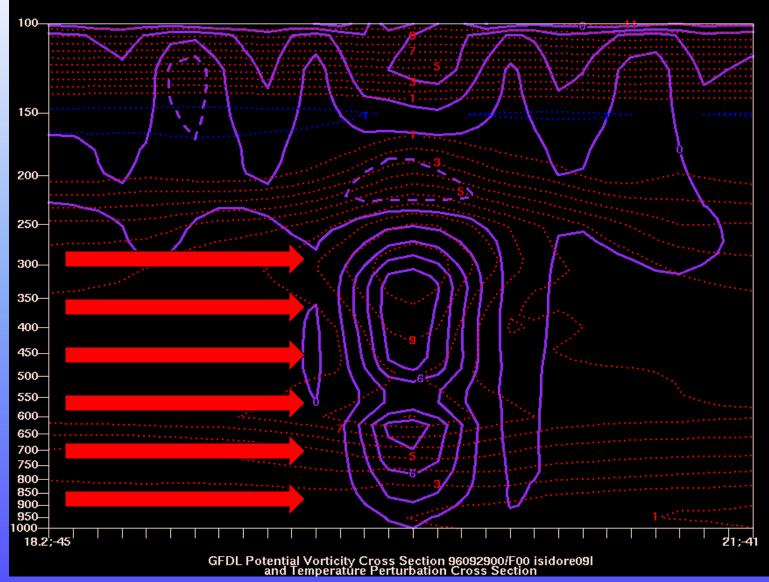






Isidore (1996)



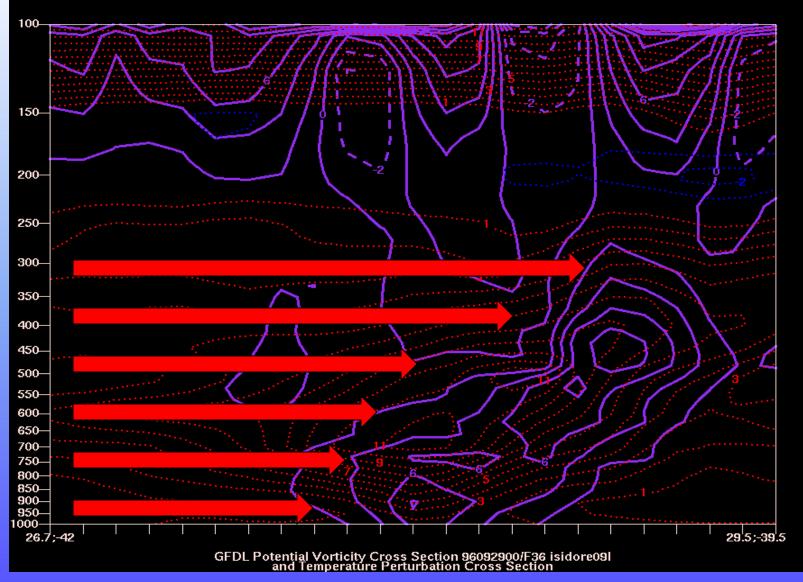


Vertical cross-section of PV (purple) and temperature anomaly from the GFDL model for the initialization of the 0000 UTC forecast on September 29



Isidore (1996)

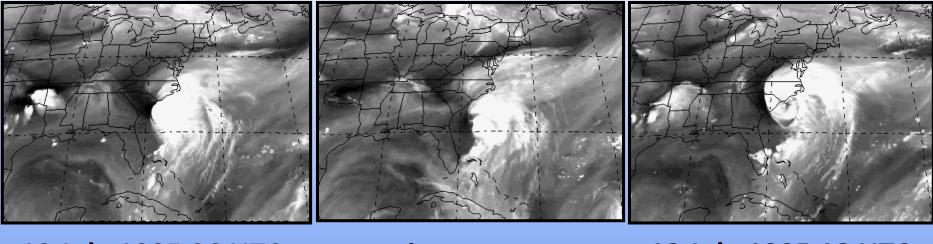




Vertical cross-section of PV (purple) and temperature anomaly from the 36-hour forecast GFDL model for the initialization of the 0000 UTC forecast on September 29

Hurricane-Trough Interaction

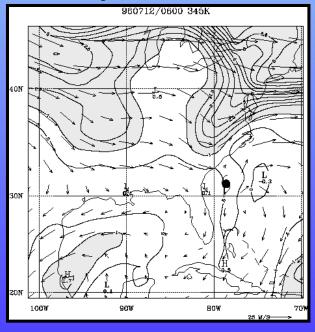
Hurricane Bertha (1996)

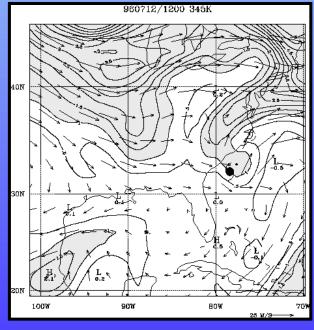


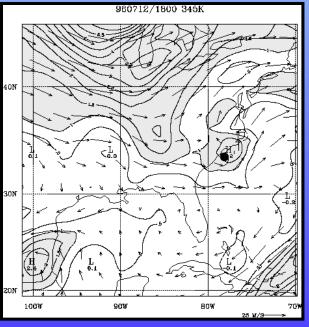
12 July 1995 06 UTC

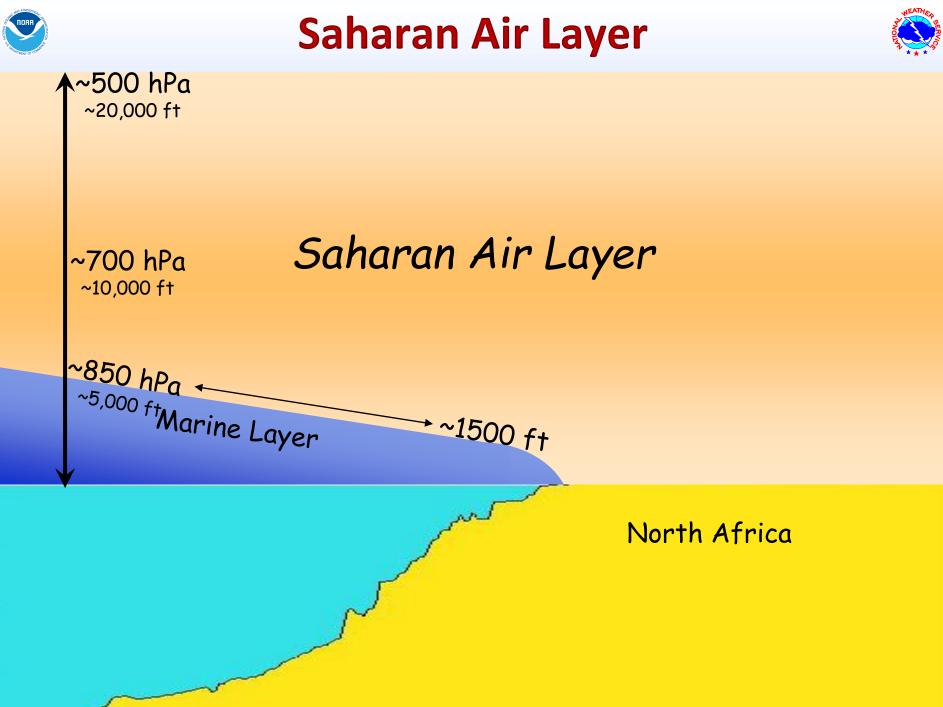
12 July 1995 12 UTC

12 July 1995 18 UTC





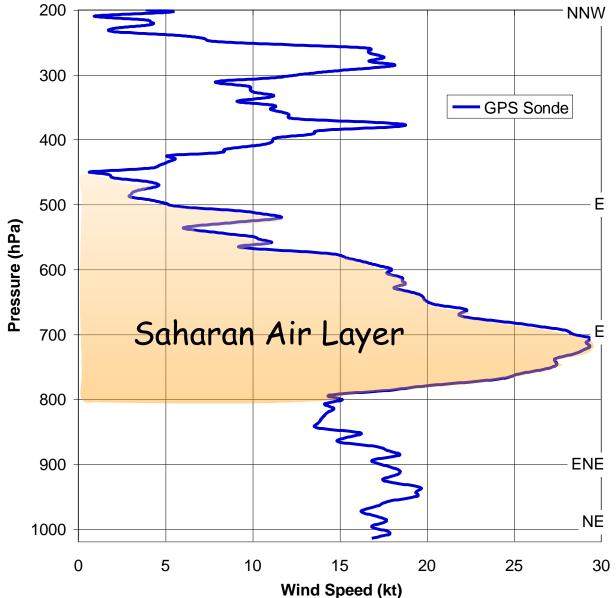


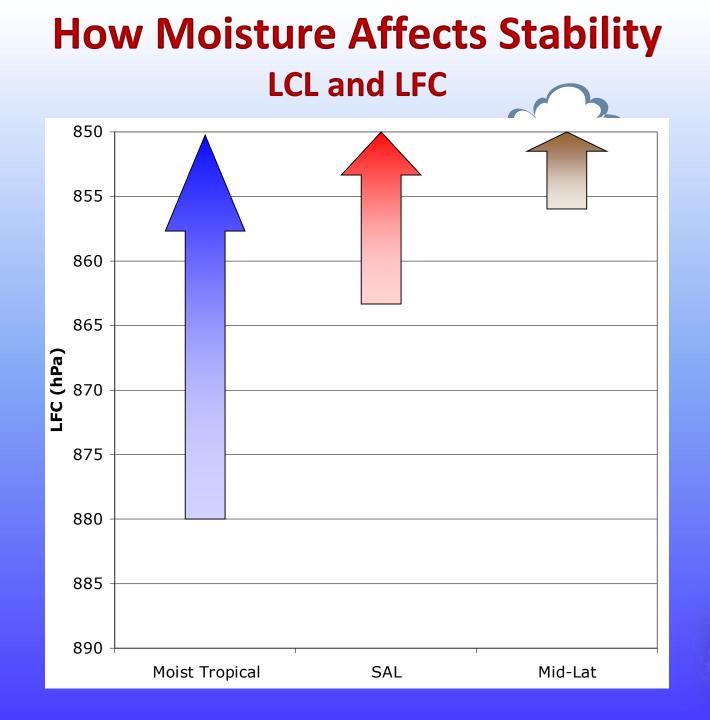


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#### **Getting Dry Air into the TC Circulation**

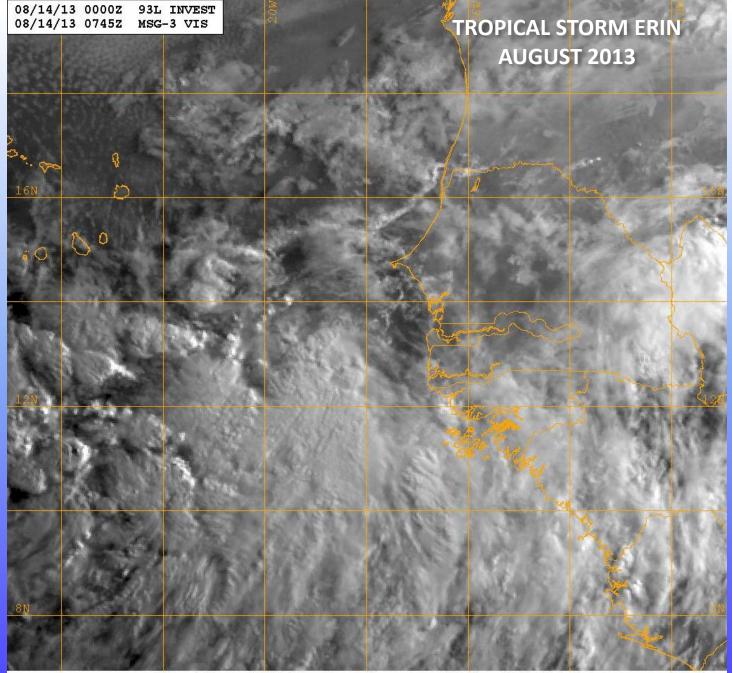












Naval Research Lab http://www.nrlmry.navy.mil/sat\_products.html <-- Visible ( Sun elevation at center is 11 degrees) -->

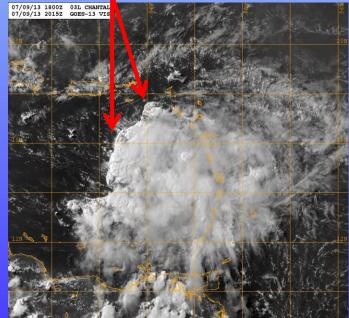
### **Influence of Dry Air on TC intensity**



In addition to its stabilizing effect, dry air at the middle levels will result in increased evaporative cooling.

This causes an increase in cold downdrafts, and low-level divergence – which should lead to the weakening of the TC.

Evidence of this is often seen when, in visible satellite images, one can see arc clouds emanating from the storm.









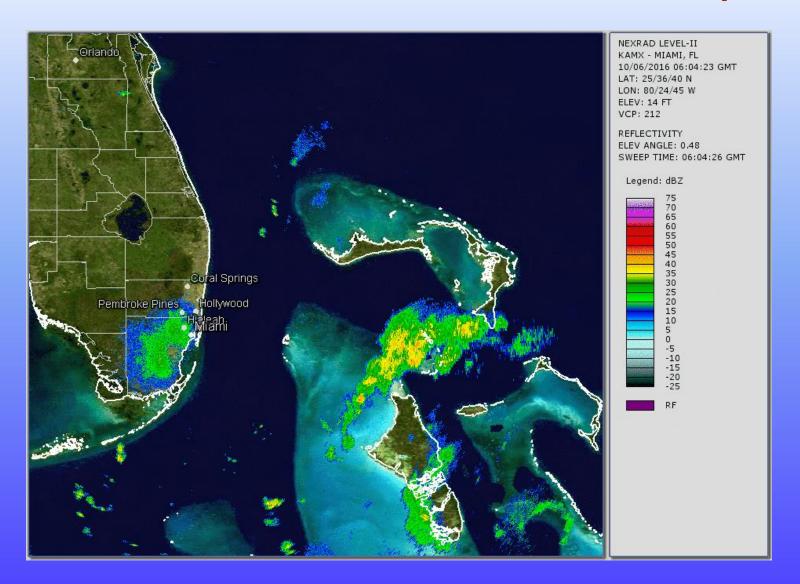
In addition to large-scale environmental influences, tropical cyclone intensity change can be caused by inner-core processes, such as eyewall replacement cycles:

In stronger hurricanes, we often see a concentric eyewall develop at a larger distance from the center than the radius of the original eyewall.

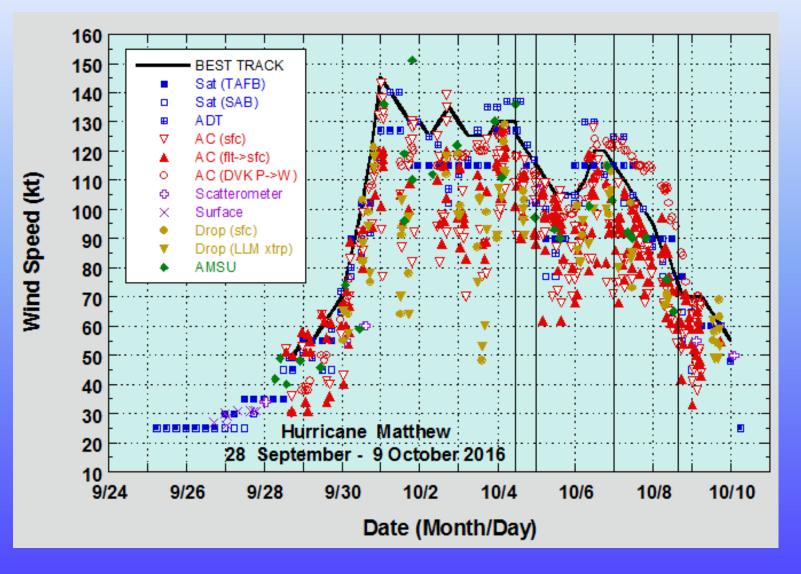
When this outer eyewall becomes dominant, some weakening usually occurs.

However, this outer eyewall could contract, in which case the hurricane would re-intensify.

### Hurricane Matthew Radar Loop



### Hurricane Matthew Maximum Wind





#### **Land Interaction**



- In general, winds weaken over land due to lack of latent heating and increased friction
- Strong winds move inland farther if the TC is moving faster
- Terrain can cause significant local "speed-ups" (sometimes by more than 10 – 30%) over hills, valleys, etc.
- Higher elevations in mountainous areas can have stronger winds than at sea level – common on Caribbean islands





## Weather Forecast Methods<sup>1</sup>

- Classical Statistical Models
  - Use observable parameters to statistical predict future evolution
- Numerical Weather Prediction (NWP)
   Physically based forecast models
- Statistical-Dynamical Models
  - Use NWP forecasts and other input for statistical prediction of desired variables
    - Station surface temperature, precipitation, hurricane intensity changes



### Tropical Cyclone Intensity Forecast Models



#### • Statistical Models:

- **Decay SHIFOR** (Statistical Hurricane Intensity FOR ecast with inland decay).
  - Based on historical information climatology and persistence (uses CLIPER track).
  - Baseline for skill of intensity forecasts
- Trajectory CLIPER
  - Statistically estimate track and intensity tendency instead of change over fixed time
    - e.g., dV/dt instead of V(t)-V(0)

#### • Statistical-Dynamical Models:

- **SHIPS** and **DSHIPS** (Statistical <u>Hurricane Intensity Prediction Scheme</u>):
  - Based on climatology, persistence, and statistical relationships to current and forecast environmental conditions (with inland decay applied in DSHIPS)
- **LGEM** (Logistic Growth Equation Model):
  - Uses same inputs as SHIPS, but environmental conditions are variable over the length of the forecast (SHIPS averages over the entire forecast)
  - More sensitive to environmental changes

#### • Dynamical Models:

– HWRF, GFDL, COAMPS-TC, GFS, UKMET, NOGAPS, ECMWF

# **Overview of the SHIPS Model**

- Multiple linear regression
  - $-y = a_0 + a_1 x_1 + \dots a_N x_N$ 
    - y = intensity change at given forecast time

 $-(V_6-V_0), (V_{12}-V_0), \dots, (V_{120}-V_0)$ 

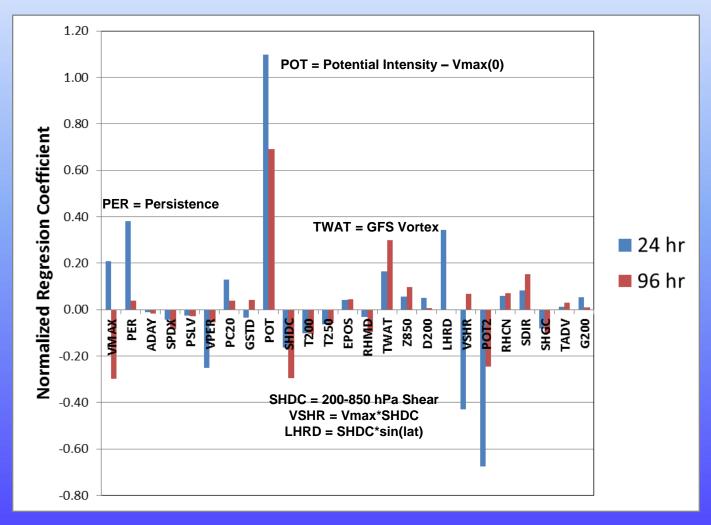
- x<sub>i</sub> = predictors of intensity change
- a<sub>i</sub> = regression coefficients
- Different coefficients for each forecast time
- Predictors x<sub>i</sub> averaged over forecast period
- x,y normalized by subtracting sample mean, dividing by standard deviation

# **SHIPS Predictors**

- 1. Climatology (days from peak)
- 2.  $V_0$  (V<sub>max</sub> at t= 0 hr)
- 3. Persistence  $(V_0 V_{-12})$
- 4. V<sub>0</sub> \* Per
- 5. Zonal storm motion
- 6. Steering layer pressure
- 7. %IR pixels  $< -20^{\circ}$ C
- 8. IR pixel standard deviation
- 9. Max Potential Intensity  $V_0$
- 10. Square of No. 9
- 11. Ocean heat content
- 12. T at 200 hPa
- 13. T at 250 hPa
- 14. RH (700-500 hPa)
- 15.  $\theta_e$  of sfc parcel  $\theta_e$  of env

- 16. 850-200 hPa env shear
- 17. Shear \*  $V_0$
- 18. Shear direction
- 19. Shear\*sin(lat)
- 20. Shear from other levels
- 21. 0-1000 km 850 hPa vorticity
- 22. 0-1000 km 200 hPa divergence
- 23. GFS vortex tendency
- 24. Low-level T advection
- 25. GFS vortex warm core

# SHIPS Regression Coefficients at 24 and 96 hr



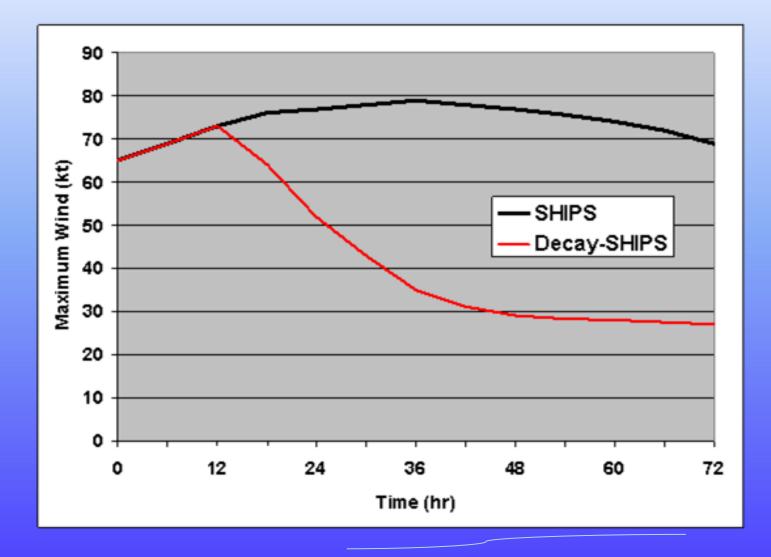
# **Impact of Land**

- Detect when forecast track crosses land
- Replace multiple regression prediction with

dV/dt = - μ(V-V<sub>b</sub>) μ = climatological decay rate ~ 1/10 hr<sup>-1</sup> V<sub>b</sub> = background intensity over land • Decay rate reduced if area within 1 deg lat

is partially over water

# **Example of Land Effect**



# **Limitations of SHIPS**

- V predictions can be negative
- Most predictors averaged over entire forecast period
  - Slow response to changing synoptic environment
- Strong cyclones that move over land and back over water can have low bias
- Logistic Growth Equation Model (LGEM) relaxes these assumptions

#### **Operational LGEM Intensity Model**

$$dV/dt = \kappa V - \beta (V/V_{mpi})^{n}V$$
(A) (B)

V<sub>mpi</sub> = Maximum Potential Intensity estimate

**κ** = Max wind growth rate (from SHIPS predictors)

 $\beta$ , n = empirical constants = 1/24 hr, 2.5

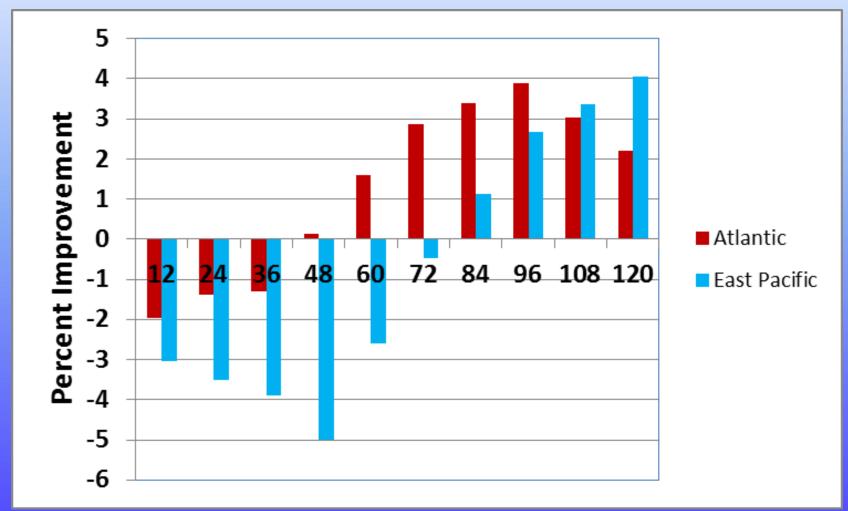
Steady State Solution:  $V_s = V_{mpi}(\beta/\kappa)^{1/n}$ 

# **LGEM versus SHIPS**

#### Advantages

- Prediction equation bounds the solution between 0 and  $V_{mpi}$
- Time evolution of predictors (Shear, etc) better accounted for
- Movement between water and land handled better because of time stepping
- Disadvantages
  - Model fitting more involved
  - Inclusion of persistence more difficult

# LGEM Improvement over SHIPS AL and EP/CP Operational Runs 2006-2016





## **SHIPS Diagnostic File**



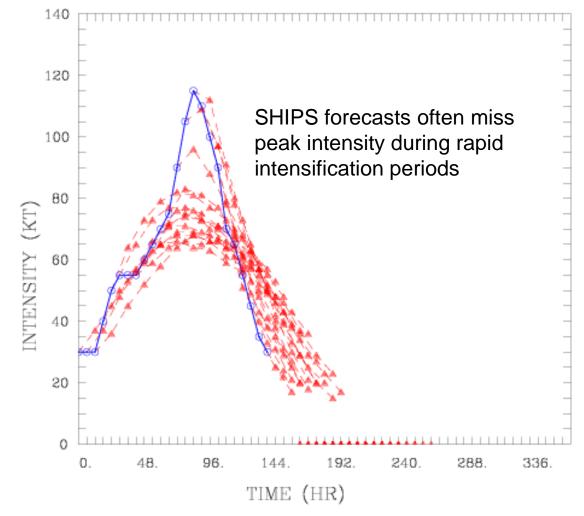
| * ATLANTIC SHIPS INTENSITY FORECAST *<br>* IR SAT DATA AVAILABLE, OHC AVAILABLE *<br>* HERMINE AL092016 09/01/16 00 UTC * |       |       |       |         |       |       |       |       |       |       |        |       |       |
|---------------------------------------------------------------------------------------------------------------------------|-------|-------|-------|---------|-------|-------|-------|-------|-------|-------|--------|-------|-------|
| TIME (HR)                                                                                                                 | 0     | 6     | 12    | 18      | 24    | 36    | 48    | 60    | 72    | 84    | 96     | 108   | 120   |
| V (KT) NO LAND                                                                                                            |       | 54    | 58    | 63      | 67    | 75    | 82    | 82    | 80    | 76    | 61     | 52    | 44    |
| V (KT) LAND                                                                                                               | 50    | 54    | 58    | 63      | 67    |       | 37    | 30    | 31    | 28    | DIS    | DIS   | DIS   |
| V (KT) LGEM                                                                                                               | 50    | 55    | 60    | 65      | 70    | 60    | 38    | 31    | 28    | 30    | 26     | 24    | 25    |
| Storm Type                                                                                                                | TROP  | TROP  |       |         | TROP  |       |       | TROP  | TROP  | TROP  | TROP   | TROP  | TROP  |
| SHEAR (KT)                                                                                                                | 13    | 13    | 10    | 10      | 13    | 15    | 26    | 39    | 49    | 39    | 28     | 22    | 19    |
| SHEAR ADJ (KT)                                                                                                            | -2    | 1     | 5     | 1       | 0     | -2    | 2     | 0     | 0     | -6    | -4     | -3    | -4    |
| SHEAR DIR                                                                                                                 | 301   | 303   | 285   | 258     | 236   | 257   | 238   | 241   | 229   | 216   | 247    | 251   | 240   |
| SST (C)                                                                                                                   | 30.4  | 30.3  | 30.2  | 30.2    | 30.2  | 29.9  | 29.2  | 28.7  | 27.5  | 26.8  | 26.5   | 26.1  | 26.1  |
| POT. INT. (KT)                                                                                                            | 170   | 170   | 171   | 172     | 172   | 169   | 157   | 149   | 131   | 120   | 116    | 113   | 114   |
| ADJ. POT. INT.                                                                                                            | 157   | 153   | 153   | 154     | 153   | 150   | 139   | 129   | 109   | 97    | 93     | 92    | 93    |
| 200 MB T (C)                                                                                                              | -51.3 | -51.7 | -52.0 | -51.5   | -51.3 | -51.6 | -50.9 | -51.4 | -51.9 | -53.1 | -53.1  | -53.1 | -53.1 |
| 200 MB VXT (C)                                                                                                            | 1.0   | 1.2   | 0.8   | 0.3     | 0.4   | 0.7   | 0.9   | 1.1   | 1.0   | 0.5   | 1.2    | 1.7   | 1.4   |
| TH_E DEV (C)                                                                                                              | 10    | 9     | 9     | 10      | 10    | 5     | 6     | 2     | 3     | 0     | 1      | 1     | 4     |
| 700-500 MB RH                                                                                                             | 64    | 62    | 64    | 64      | 66    | 65    | 56    | 46    | 49    | 53    | 52     | 52    | 46    |
| MODEL VTX (KT)                                                                                                            | 17    | 18    | 20    | 22      | 23    | 25    | 28    | 27    | 28    | 30    | 22     | 20    | 17    |
| 850 MB ENV VOR                                                                                                            | 44    | 28    | 33    | 45      | 53    | 41    | 44    | 9     | -3    | 2     | 9      | 17    | 16    |
| 200 MB DIV                                                                                                                | 30    | 24    | 48    | 56      | 78    | 71    | 90    | 58    | 62    | 43    | 46     | 6     | 14    |
| 700-850 TADV                                                                                                              | 7     | 15    | 16    | 14      | 12    | 20    | 21    | 42    | 9     | -5    | 3      | -2    | -2    |
| LAND (KM)                                                                                                                 | 440   | 414   | 334   | 219     | 112   | -62   | -50   | -96   | 7     | 61    | 96     | 179   | 246   |
| LAT (DEG N)                                                                                                               | 25.5  | 26.2  | 26.8  | 27.8    | 28.7  | 30.5  | 32.7  | 35.0  | 37.1  | 38.4  | 38.7   | 39.0  | 39.1  |
| LONG(DEG W)                                                                                                               | 87.1  | 86.7  | 86.3  | 85.7    | 85.2  | 83.6  | 81.0  | 78.3  | 75.8  | 74.3  | 73.7   | 72.4  | 70.5  |
| STM SPEED (KT)                                                                                                            | 8     | 7     | 9     | 11      | 11    | 13    | 16    | 15    | 12    | 6     | 4      | 6     | 8     |
| HEAT CONTENT                                                                                                              | 38    | 35    | 37    | 41      | 37    | 43    | 37    | 47    | 1     | 41    | 1      | 2     | 1     |
| FORECAST TRACK FROM OFCI INITIAL HEADING/SPEED (DEG/KT): 25/ 8 CX,CY: 3/ 7                                                |       |       |       |         |       |       |       |       |       |       |        |       |       |
| T-12 MAX WINE                                                                                                             |       |       |       | PRESSUR |       |       |       |       |       |       | N=618) | )     |       |
| GOES IR BRIGH                                                                                                             |       |       |       |         |       |       |       |       |       |       |        |       |       |
| % GOES IR PIXELS WITH T < -20 C 50-200 KM RAD: 67.0 (MEAN=65.0)                                                           |       |       |       |         |       |       |       |       |       |       |        |       |       |

14.8

Available in real time from ftp://ftp.nhc.noaa.gov/atcf/stext

PRELIM RI PROB (DV .GE. 30 KT IN 24 HR):

# SHIPS Forecasts For East Pacific Hurricane Georgette (2016)



# **The Rapid Intensification Index**

- Define RI as 30 kt or greater intensity increase in 24 hr
- Find subset of SHIPS predictors that separate RI and non-RI cases
- Use training sample to convert discriminant function value to a probability of RI
- AL and EP/CP versions include more thresholds (25, 30, 35, 40 kt changes, etc)

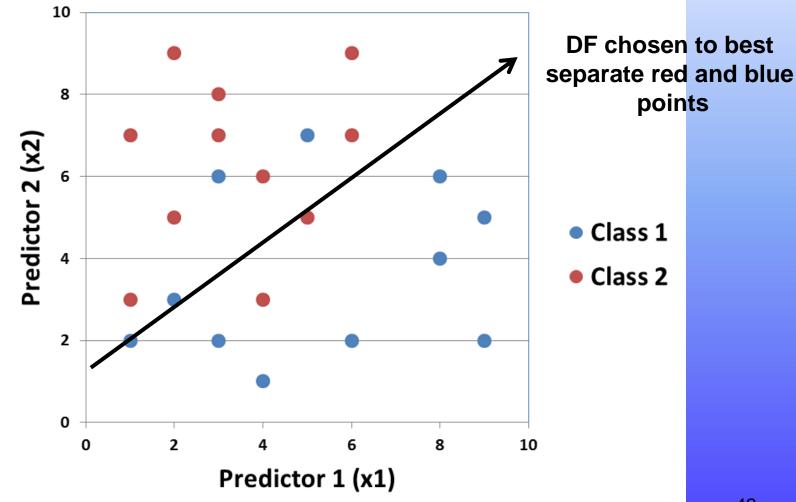
# **Linear Discriminant Analysis**

- 2 class example
  - Objectively determine which of two classes a data sample belongs to
    - Rapid intensifier or non-rapid intensifier
  - Predictors for each data sample provide input to the classification
- Discriminant function (DF) linearly weights the inputs

 $DF = a_0 + a_1 x_1 + \dots a_N x_N$ 

 Weights chosen to maximize separation of the classes

# Graphical Interpretation of the Discriminant Function



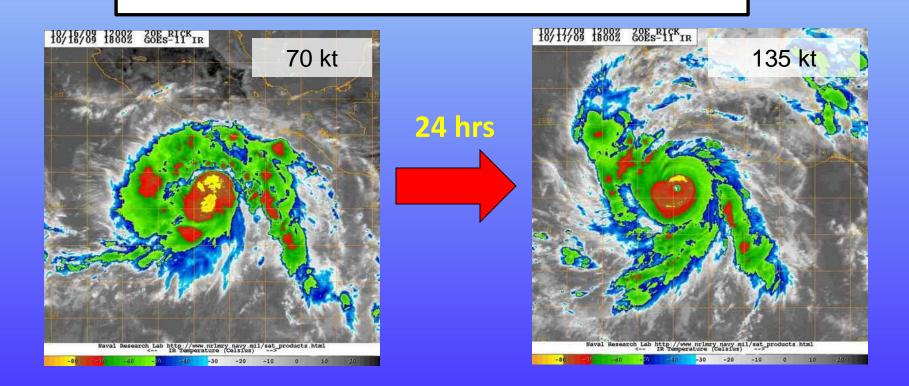
# **RII Discriminators**

- 1. Previous 12 h max wind change (persistence)
- 2. Maximum Potential Intensity Current intensity
- 3. Oceanic Heat Content
- 4. 200-850 hP shear magnitude (0-500 km)
- 5. 200 hPa divergence (0-1000 km)
- 6. 850-700 hPa relative humidity (200-800 km)
- 7. 850 hPa tangential wind (0-500 km)
- 8. IR pixels colder than -30°C
- 9. Azimuthal standard deviation of IR brightness temperature



### **Rapid Intensification** Hurricane Rick (2009 - East Pacific)

|       | FORECAS | T POSITIO | NS AND | MAX WIN | IDS |    |
|-------|---------|-----------|--------|---------|-----|----|
| INITI | AL      | 16/2100z  | 13.0N  | 100.0W  | 75  | KT |
| 12HR  | VT      | 17/0600z  | 13.2N  | 101.3W  | 90  | KT |
| 24hr  | VT      | 17/1800Z  | 13.7N  | 103.3W  | 105 | KT |
| 36hr  | VT      | 18/0600Z  | 14.3N  | 105.8W  | 115 | KT |
| 48HR  | VT      | 18/1800Z  | 15.0N  | 108.1W  | 125 | KT |
| 72HR  | VT      | 19/1800Z  | 16.5N  | 111.5W  | 120 | KT |
| 96HR  | VT      | 20/1800Z  | 18.5N  | 113.OW  | 105 | KT |
| 120HR | VT      | 21/1800Z  | 20.5N  | 113.OW  | 85  | KT |
|       |         |           |        |         |     |    |



## **RI Guidance**



#### Hurricane Rick (2009 - East Pacific)

|                | * E         | AST PACIE | FIC SHIPS | S INTEN | SITY F | ORECAS | r *      |      |        |       |     |
|----------------|-------------|-----------|-----------|---------|--------|--------|----------|------|--------|-------|-----|
|                | *           | GOES DA   | ATA AVAII | LABLE   |        |        | *        |      |        |       |     |
|                | *           | OHC D     | ATA AVAI  | LABLE   |        |        | *        |      |        |       |     |
|                | * R         | ICK       | EP2020    | 09 10/  | /16/09 | 18 UT  | 'C *     |      |        |       |     |
|                |             |           |           |         |        |        |          |      |        |       |     |
| TIME (HR)      | 0 6         | 12 1      | 8 24      | 36      | 48     | 60     | 72       | 84   | 96     | 108   | 120 |
| V (KT) NO LAND | 70 79       | 86 9      | 2 97      | 104     | 108    | 111    | 111      | 107  | 107    | 101   | 93  |
| V (KT) LAND    | 70 79       | 86 9      | 2 97      | 104     | 108    | 111    | 111      | 107  | 107    | 101   | 93  |
| V (KT) LGE mod | 70 79       | 86 9      | 2 96      | 99      | 95     | 91     | 87       | 85   | 83     | 80    | 76  |
|                |             |           |           |         |        |        |          |      |        |       |     |
| ** 20          | 09 E. Paci  | fic RI IN | DEX EP20  | 2009 RI | ICK    | 10/    | 16/09    | 18 U | JTC ** |       |     |
|                | (           | 30 KT OF  | R MORE MA | AX WIND | INCRE  | ASE IN | NEXT 2   | 4 HR | )      |       |     |
|                |             |           |           |         |        |        |          |      |        |       |     |
| 12 HR PERSI    |             |           | Range:-2  |         |        |        | -        |      |        | 1.6   |     |
| 850-200 MB     |             |           | 2         |         |        |        | 2        |      |        |       |     |
| D200 (10**7    |             |           | Range:-1  |         |        |        | -        |      |        |       |     |
| POT = MPI-V    |             |           | Range: 4  |         |        |        | -        |      |        |       |     |
| 850-700 MB     |             |           | -         |         |        |        | -        |      |        | 0.2   |     |
| % area w/pi    |             |           | -         |         |        |        | -        |      |        | 0.5   |     |
| STD DEV OF     |             |           | 2         |         |        |        | 2        |      |        | 1.3   |     |
| Heat conter    | nt (KJ/cm2) | : 46.8    | Range:    | 4.0 to  | 67.0   | Scaled | l/Wgted  | Val: | : 0.7/ | 0.4   |     |
|                |             |           |           |         |        |        |          |      |        |       |     |
| Prob of RI     |             |           |           | 78% is  |        |        |          |      | mean(1 |       |     |
| Prob of RI     |             |           |           | 71% is  |        |        |          |      | mean(  |       |     |
| Prob of RI     | for 35 kt   | RI thresh | old=      | 66% is  | 12.6   | times  | the same | mple | mean(  | 5.2%) |     |



WEATHER SERVICE

CURRENT MAX WIND (KT): 50. LAT, LON: 25.5 87.1

\*\* 2015 ATLANTIC RI INDEX AL092016 HERMINE 09/01/16 00 UTC \*\* (SHIPS-RII PREDICTOR TABLE for 30 KT OR MORE MAXIMUM WIND INCREASE IN NEXT 24-h)

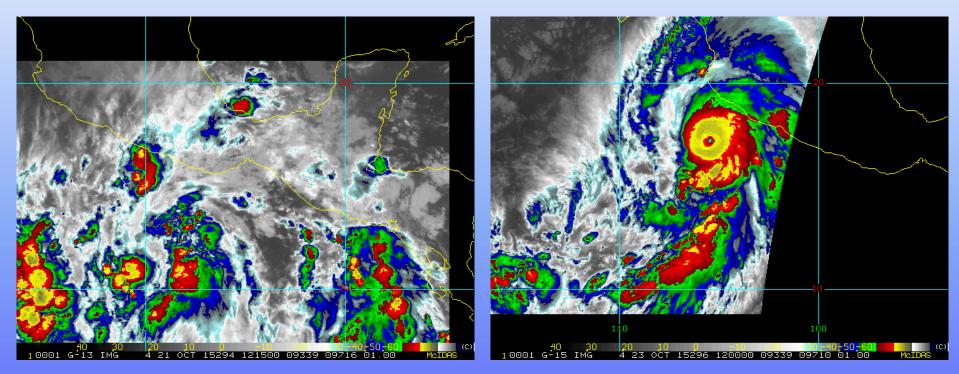
| alue – RI Predi | .ctor Kange                                                                                                                                                                                                                                                                                                                                                                                      | - Scaled Value(U-)                                   | 1) % Contribution                                    |
|-----------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|
| 10.0 -49.5      | to 33.0                                                                                                                                                                                                                                                                                                                                                                                          | 0.72                                                 | 4.6                                                  |
| 11.9 28.8       | to 2.9                                                                                                                                                                                                                                                                                                                                                                                           | 0.65                                                 | 1.9                                                  |
| 37.6 0.0        | to 155.1                                                                                                                                                                                                                                                                                                                                                                                         | 0.24                                                 | 0.5                                                  |
| 23.8 37.5       | to 2.9                                                                                                                                                                                                                                                                                                                                                                                           | 0.40                                                 | 1.1                                                  |
| 0.4 2.8         | to -3.1                                                                                                                                                                                                                                                                                                                                                                                          | 0.41                                                 | 1.1                                                  |
| 50.0 22.5       | to 121.0                                                                                                                                                                                                                                                                                                                                                                                         | 0.78                                                 | 0.8                                                  |
| 47.2 -23.1      | to 181.5                                                                                                                                                                                                                                                                                                                                                                                         | 0.34                                                 | 0.4                                                  |
| 04.0 28.4       | to 139.1                                                                                                                                                                                                                                                                                                                                                                                         | 0.68                                                 | 1.1                                                  |
| 0.0 100.0       | to 0.0                                                                                                                                                                                                                                                                                                                                                                                           | 1.00                                                 | 0.7                                                  |
| 43.4 960.3      | to -67.1                                                                                                                                                                                                                                                                                                                                                                                         | 0.80                                                 | 0.0                                                  |
| r RI thresholds | 7% is                                                                                                                                                                                                                                                                                                                                                                                            | 1 3 times comple                                     | mean $(5.5\%)$                                       |
|                 |                                                                                                                                                                                                                                                                                                                                                                                                  | -                                                    | · ·                                                  |
|                 |                                                                                                                                                                                                                                                                                                                                                                                                  |                                                      |                                                      |
|                 |                                                                                                                                                                                                                                                                                                                                                                                                  |                                                      |                                                      |
| 1132 940 4 rrr  | .0.0       -49.5         .1.9       28.8         .7.6       0.0         .23.8       37.5         0.4       2.8         50.0       22.5         .7.2       -23.1         .4.0       28.4         0.0       100.0         .3.4       960.3         c       RI         threshold=         c       RI         c       RI         threshold=         c       RI         c       RI         threshold= | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |

| SHIPS Pro | D KI for | ∙ 4UKt⁄ . | 24nr RI | threshold= | 8% IS  | 2.9 | times | sample : | mean | ( ) | 2.8%) |
|-----------|----------|-----------|---------|------------|--------|-----|-------|----------|------|-----|-------|
| SHIPS Pro | b RI for | - 45kt∕ ∶ | 36hr RI | threshold= | 10% is | 2.1 | times | sample : | mean | (   | 4.9%) |
| SHIPS Pro | b RI for | 55kt/ -   | 48hr RI | threshold= | 19% is | 3.7 | times | sample : | mean | (   | 5.1%) |

Matrix of RI probabilities

| RI (kt / h) | 20/12 | 25/24 | 30⁄24 | 35/24 | 40/24 | 45⁄36 | 55⁄48 |
|-------------|-------|-------|-------|-------|-------|-------|-------|
| SHIPS-RII:  | 7.3%  | 24.1% | 12.2% | 11.4% | 8.2%  | 10.4% | 18.8% |
| Logistic:   | 6.9%  | 28.6% | 16.2% | 8.6%  | 0.0%  | 8.5%  | 6.9%  |
| Bayesian:   | 3.1%  | 2.1%  | 0.4%  | 0.3%  | 0.1%  | 0.6%  | 0.5%  |
| Consensus:  | 5.8%  | 18.3% | 9.6%  | 6.8%  | 2.8%  | 6.5%  | 8.8%  |

#### PATRICIA INTENSIFIED FROM 40 KT TO 185 KT IN 48 HOURS!



#### 21 OCT 2015 12 UTC

#### 23 OCT 2015 12 UTC





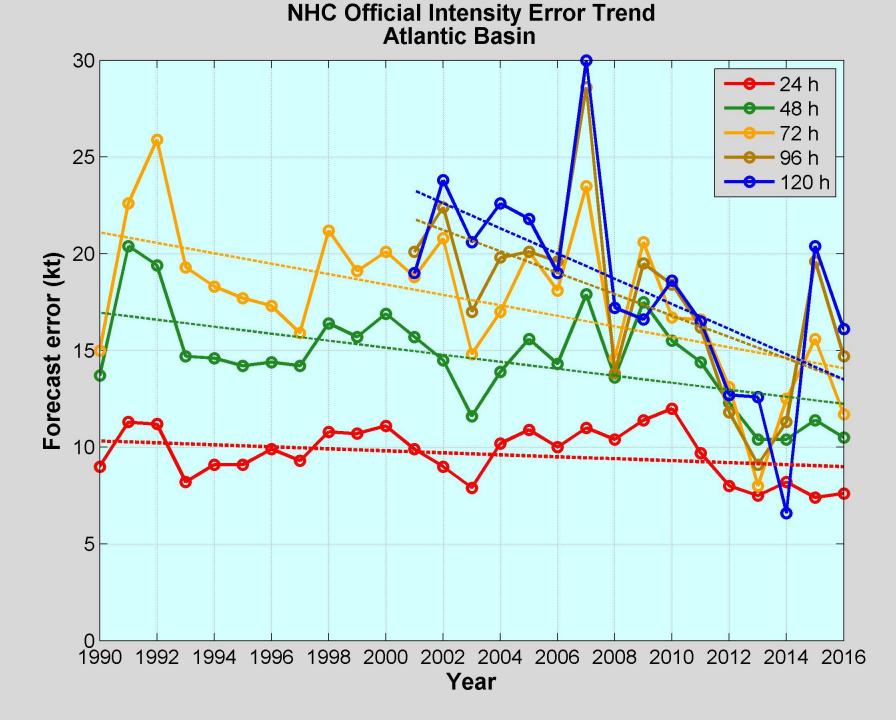


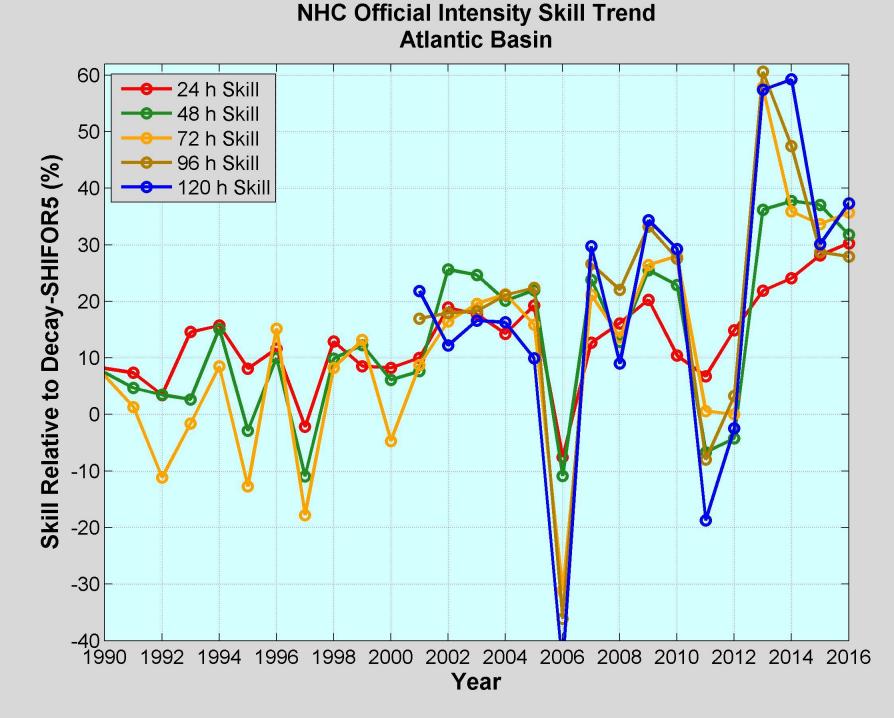
- HWRF, GFDL, NCEP Global Model (GFS), UKMET (U.K. Met Office), NOGAPS (U.S. Navy), ECMWF (European)
- These models have forecast errors due to...
  - sparse observations
  - inadequate resolution (need to go down to a few km grid spacing; the HWRF and GFDL, our highest-resolution operational hurricane models, are currently about 9 km and 2 km, respectively).
  - incomplete understanding and simulation of basic physics of intensity change.
  - problems with representation of shear.
- Steady improvements over past few years to due improved resolution, physics and data assimilation

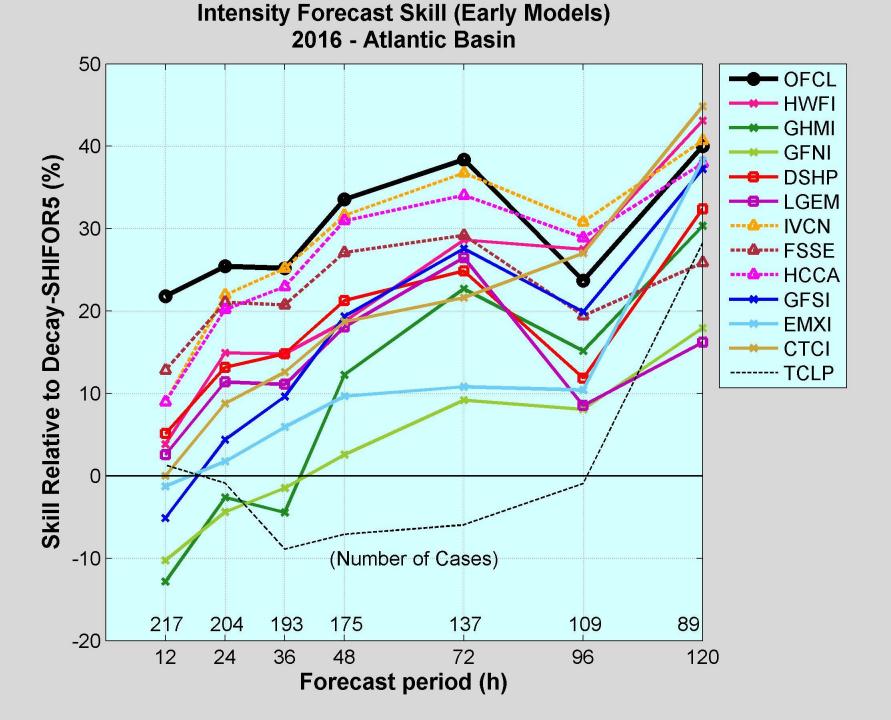
## **Consensus and Ensemble Forecasts**



- ICON Consensus that is computed by averaging the forecast intensities from Decay-SHIPS, LGEM, HWRF, and GFDL. All must be available.
- IVCN Consensus that requires at least 2 of Decay-SHIPS, LGEM, HWRF, GFDL, and GFDN.
- FSSE (Florida State Superensemble) Consensus that uses dynamical models and the previous NHC forecast. The FSSE learns from past performances of its member models in a "training phase", then accounts for the model biases.
- HCCA (HFIP Corrected Consensus Approach) FSSE approach adapted to NHC operations









# **NHC Official Intensity Forecast**



- Based on statistical guidance from SHIPS and D-SHIFOR, qualitative guidance from dynamical models and consensus.
- Dynamical models (HWRF and COTC) more skillful last few years
- Persistence is used quite a bit!
- Obvious signs in the environment, i.e. cooler waters, increasing upper-level winds, are taken into account.
- Generally corresponds to what is *normal* for a storm in any particular situation (e.g. the standard Dvorak development rate).
- Tends to be conservative; extreme events are almost never forecast.
- For forecasts 24 h and beyond, the average error is roughly 1 SSHWS Category (15-20 knots).



# **Concluding Remarks**



- Intensity forecasting is not as advanced as track forecasting.
- There is less skill for intensity forecasting than there is for track forecasting.
- Current guidance is provided mainly by DSHIPS, LGEM, GFDL, HWRF, IVCN and more recently, COAMPS-TC, FSSE and HCCA
- We still have significant difficulty in forecasting rapidly intensifying and rapidly weakening storms.
- The main hope for the future lies in improved dynamical models, coupled with enhanced observations and understanding of the hurricane's inner core. Hurricane Forecast Improvement Project (HFIP)

 GOES-16 will provide new imagery and lightning data for dynamical and statistical-dynamical intensity models

# EXERCISE 2 Intensity Forecast